

FRIEDRICH-SCHILLER-UNIVERSITÄT JENA
PHYSIKALISCH-ASTRONOMISCHE-FAKULTÄT



**FRIEDRICH-SCHILLER-
UNIVERSITÄT
JENA**

PROF. MARKUS SCHMIDT

Fiber Optics

All Exercises

Summer term 2022

Name: MARTIN BEYER

Contents

1	Mirror waveguide	3
1.1	Wave equation for TE-polarization	3
1.2	Wave equation for TM-polarization	4
1.3	Dispersion equation for TE-polarization	5
1.4	Propagation constant	6
1.5	Group velocity dispersion	7
2	The symmetric planar slab waveguide	8
2.1	Derivation of γ_1, γ_3 and κ	8
2.2	Boundary conditions	9
2.3	Dispersion relation	9
2.4	Effective indices	10
2.5	Poynting vector	10
3	Optical fiber	12
3.1	Transverse EM-components	12
3.2	Application of boundary conditions	13
3.3	Dispersion relation	14
4	Weakly guiding fibers	16
4.1	Cut-off condition	16
4.2	Cut-off numbers	16
4.3	Effective index	17
4.4	Group velocity	18
5	Pulse propagation	19
5.1	Pulse envelope without dispersion	19
5.2	Pulse envelope with dispersion	20
5.3	Pulse width	20
5.4	Cross over position for different initial pulse lengths	21

1 Mirror waveguide

The slab mirror waveguide relies on a symmetrically embedded high refractive index film (dispersionless, refractive index n , film thickness d) sandwiched between two perfect metals.

1.1 Wave equation for TE-polarization

Derive the wave equation for the mirror waveguide in TE-polarization for the y -component (in Cartesian coordinates) of the electric field assuming:

- a harmonic ansatz
- translational invariance along the y -direction
- propagation along the z -direction
- TE-condition: $E_x = E_z = H_y = 0$

Solution:

Using the assumptions above we can formulate an ansatz for the electric field amplitude

$$\mathbf{E}(x, y, z) = E_y(x, z)e^{i\beta z}e^{-i\omega t}\hat{\mathbf{e}}_y. \quad (1.1)$$

Now we can use Maxwells equations

$$\vec{\nabla} \times \mathbf{E} = -\frac{\partial}{\partial t}\mu_0\mathbf{H} \quad \text{and} \quad \vec{\nabla} \times \mathbf{H} = \frac{\partial}{\partial t}\mathbf{D} = \epsilon_0\epsilon\frac{\partial}{\partial t}\mathbf{E} \quad (1.2)$$

to derive the wave equation. Applying the curl to Faradays law gives us

$$\begin{aligned} \vec{\nabla} \times (\vec{\nabla} \times \mathbf{E}) &= \vec{\nabla} \underbrace{(\vec{\nabla} \cdot \mathbf{E})}_{=0} - \Delta \mathbf{E} \stackrel{(1.2)}{=} -\mu_0 \frac{\partial}{\partial t} (\vec{\nabla} \times \mathbf{H}) \\ &= -\underbrace{\mu_0 \epsilon_0 \epsilon}_{1/c_0^2} \frac{\partial^2}{\partial t^2} \mathbf{E}. \end{aligned} \quad (1.3)$$

Using the harmonic ansatz of the electric field we can substitute the time derivative with " $-i\omega$ " and find

$$\begin{aligned} \left(\Delta + \epsilon \frac{\omega^2}{c_0^2} \right) \mathbf{E}(x, y, z) &= 0 \\ \left(\Delta_t - \beta^2 + \epsilon \frac{\omega^2}{c_0^2} \right) E_y(x, z) &= 0. \end{aligned} \quad (1.4)$$

1.2 Wave equation for TM-polarization

Derive a similar wave equation in case of TM-polarization for the y -component of the magnetic field using the same assumption and the polarization conditions complementary to the TE-conditions.

Solution:

We now need to consider the magnetic field \mathbf{H} . Similar to equation (1.3) we take the curl on Amperes law

$$\begin{aligned}\vec{\nabla} \times (\vec{\nabla} \times \mathbf{H}) &= \vec{\nabla} \underbrace{(\vec{\nabla} \cdot \mathbf{H})}_{=0} - \Delta \mathbf{H} \stackrel{(1.2)}{=} \epsilon_0 \epsilon \frac{\partial}{\partial t} (\vec{\nabla} \times \mathbf{E}) \\ &= - \underbrace{\mu_0 \epsilon_0 \epsilon}_{1/c_0^2} \frac{\partial^2}{\partial t^2} \mathbf{H}.\end{aligned}\tag{1.5}$$

Analogously to the task before we can then derive the wave equation as

$$\left(\Delta_t - \beta^2 + \epsilon \frac{\omega^2}{c_0^2} \right) H_y(x, z) = 0.\tag{1.6}$$

1.3 Dispersion equation for TE-polarization

Use the following ansatz for the modal fields to find the dispersion equation in TE-polarization taking into account the boundary conditions

$$E_y = E_y^0 \cos(k_{\perp} x) \quad \text{and} \quad E_y \left(x = \pm \frac{d}{2} \right) = 0. \quad (1.7)$$

What happens to the dispersion relation in case of the anti-symmetric mode?

Solution:

Substituting ansatz (1.7) into (1.4) yields

$$\left(\Delta_t - \beta^2 + \varepsilon \frac{\omega^2}{c_0^2} \right) E_y^0 \cos(k_{\perp} x) = \left(-k_{\perp}^2 - \beta^2 + \varepsilon \frac{\omega^2}{c_0^2} \right) E_y^0 \cos(k_{\perp} x) = 0. \quad (1.8)$$

In order to always fulfill this equation the following must hold:

$$k_{\perp}^2 + \beta^2 = \varepsilon \frac{\omega^2}{c_0^2} := k^2 \quad \text{with} \quad k = nk_0. \quad (1.9)$$

Using the boundary condition we have

$$\begin{aligned} \cos\left(\pm k_{\perp} \frac{d}{2}\right) = 0 &\Rightarrow k_{\perp} \frac{d}{2} = \frac{\pi}{2} + n\pi \quad \text{with} \quad n \in \mathbb{N}_0 \\ &\Rightarrow k_{\perp} = \frac{2}{d} \pi \left(n + \frac{1}{2} \right) = \frac{\pi}{d} m \quad \text{with} \quad m = 1, 3, 5, \dots \end{aligned} \quad (1.10)$$

Then we can solve (1.9) for β and find

$$\beta = \sqrt{k^2 - k_{\perp}^2} = \sqrt{n^2 k_0^2 - \left(\frac{\pi}{d} m \right)^2} = nk_0 \sqrt{1 - \left(\frac{m\pi}{dnk_0} \right)^2}. \quad (1.11)$$

If we now introduce an effective index $n_{\text{eff}} = \frac{\beta}{k_0}$ we find the dispersion equation of a mirror waveguide

$$n_{\text{eff}} = n \sqrt{1 - \left(\frac{m\pi}{dnk_0} \right)^2} \quad \text{with} \quad m = 1, 3, 5, \dots \quad (1.12)$$

For the anti-symmetric mode m will take even values $m = 2, 4, 6, \dots$

1.4 Propagation constant

Plot the propagation constant as function of wavelength for the three lowest order modes ($n = 1.45$, $d = 2\mu\text{m}$, $0.5 < \lambda < 6\mu\text{m}$). Derive general expressions for the cut-off wavelength (at which $\beta = 0$) and plot the cut-off wavelength for the mode order (combining solution of TE- and TM-polarization) $1 \leq m \leq 5$ for the above mentioned parameters.

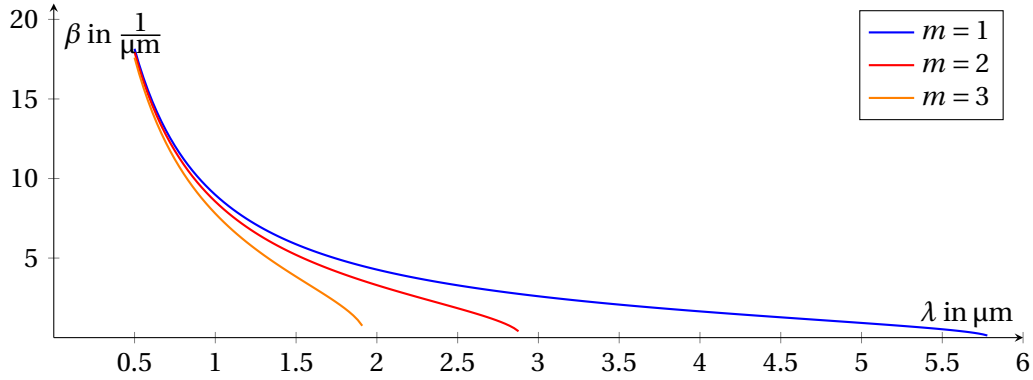


Fig. 1: Propagation constant as a function of wavelength for the three lowest order modes for a glass mirror guide.

The cut-off wavelength can be determined by setting (1.11) to zero:

$$0 = \sqrt{1 - \left(\frac{m\pi}{dnk_0}\right)^2} \Rightarrow 1 = \frac{m\lambda}{2dn} \Rightarrow \lambda_c = \frac{2dn}{m}. \quad (1.13)$$

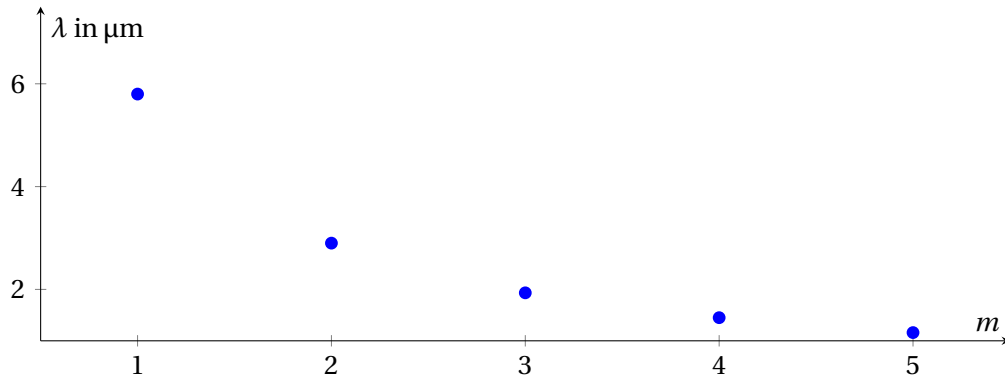


Fig. 2: Cut-off wavelength λ_c as a function of the mode order.

1.5 Group velocity dispersion

Derive analytic equations for the group velocity dispersion and show that causality holds. Plot the relative group velocity (v_g/c_0) as a function of wavelength for the configuration defined in Exercise 1.4. What happens close to the cut-off?

Solution:

The group velocity is given as

$$v_g = \frac{d\omega}{d\beta} \Rightarrow \frac{1}{v_g} = \frac{d\beta}{d\omega} = \frac{d}{d\omega} \left(\frac{n}{c} \omega \sqrt{1 - \left(\frac{m\pi c}{dn\omega} \right)^2} \right). \quad (1.14)$$

For a shorter notation we summarize the constants $\frac{m\pi c}{dn}$ into a new constant α . Then we can formally calculate the derivative¹

$$\frac{d\beta}{d\omega} = \frac{n}{c} \left(\sqrt{1 - \frac{\alpha^2}{\omega^2}} + \omega \frac{\frac{\alpha^2}{\omega^3}}{\sqrt{1 - \frac{\alpha^2}{\omega^2}}} \right) = \frac{n}{c} \frac{1}{\sqrt{1 - \frac{\alpha^2}{\omega^2}}} \left(1 - \frac{\alpha^2}{\omega^2} + \frac{\alpha^2}{\omega^2} \right) = \frac{n}{c} \frac{1}{\sqrt{1 - \frac{\alpha^2}{\omega^2}}}. \quad (1.15)$$

Thus the group velocity dispersion is

$$v_g = \frac{d\omega}{d\beta} = \left(\frac{n}{c} \frac{1}{\sqrt{1 - \frac{\alpha^2}{\omega^2}}} \right)^{-1} = \frac{c}{n} \sqrt{1 - \left(\frac{m\pi}{dnk_0} \right)^2}. \quad (1.16)$$

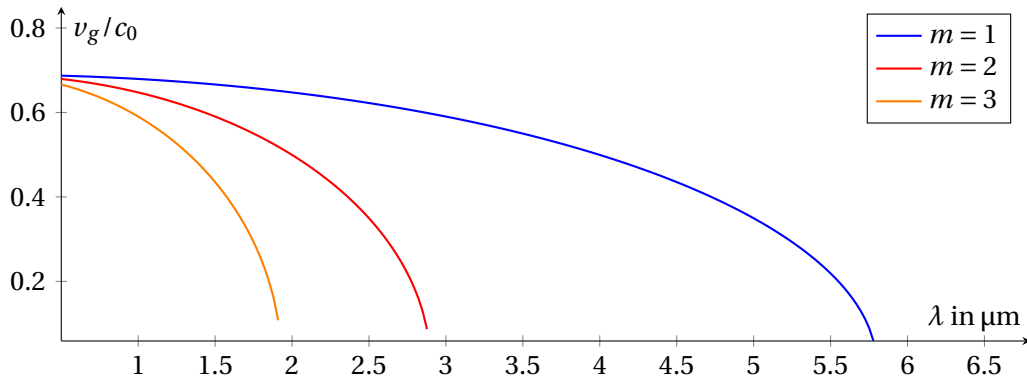


Fig. 3: Relative group velocity as a function of wavelength for the previously defined configuration. Close to the cut-off the relative velocity drops down to zero very quickly.

¹It is much easier to put ω into the square root, then we don't have to apply the product rule.

2 The symmetric planar slab waveguide

Given is a symmetric dielectric slab waveguide in TE polarization (see sketch below). The propagation direction is along the z -axis and the waveguide is invariant along the y -direction. The modes in this structure are given by:

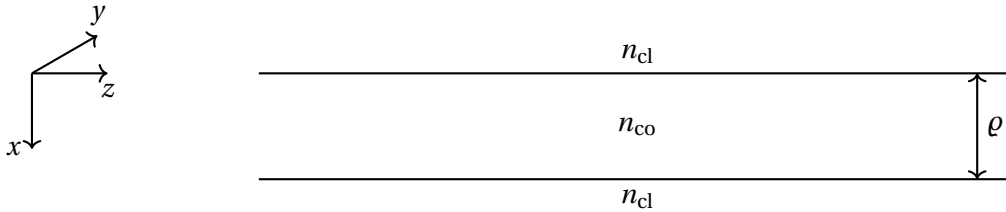


Fig. 4: Geometry of the planar slab waveguide

$$E_y = \begin{cases} Ae^{-\gamma_1(x-\rho)} & x \geq \rho \\ B \sin(\kappa x) + C \cos(\kappa x) & 0 \leq x < \rho \\ De^{\gamma_3 x} & x < 0 \end{cases} \quad (2.1)$$

2.1 Derivation of γ_1, γ_3 and κ

Use the wave equation to derive expressions for γ_1, γ_3 and κ .

Solution:

We can formulate the wave equations as follows:

$$\left(\frac{\partial^2}{\partial x^2} + n_{co}^2 k_0^2 - \beta^2 \right) E(x) = 0 \quad (2.2)$$

$$\left(\frac{\partial^2}{\partial x^2} + n_{cl}^2 k_0^2 - \beta^2 \right) E(x) = 0. \quad (2.3)$$

Using the ansatz for the fields (2.1) we can find

$$\kappa^2 = n_{co}^2 k_0^2 - \beta^2 \quad \text{and} \quad \gamma_3^2 = \gamma_1^2 = \beta^2 - n_{cl}^2 k_0^2. \quad (2.4)$$

2.2 Boundary conditions

Write down the boundary conditions for this waveguide configuration.

Solution:

The boundary conditions are obtained by demanding continuity of the transverse electric fields and their derivatives at the two interfaces. At $x = 0$ we find

$$De^{\gamma_3 0} = B \sin(\kappa 0) + C \cos(\kappa 0) \Rightarrow D = C \quad (2.5)$$

$$D\gamma_3 e^{\gamma_3 0} = B\kappa \cos(\kappa 0) - C\kappa \sin(\kappa 0) \Rightarrow D\gamma_3 = B\kappa. \quad (2.6)$$

For the boundary at $x = \rho$ we find

$$A = B \sin(\kappa \rho) + C \cos(\kappa \rho) \quad (2.7)$$

$$-A\gamma_1 = B\kappa \cos(\kappa \rho) - C\kappa \sin(\kappa \rho). \quad (2.8)$$

2.3 Dispersion relation

Derive the dispersion relation of the modes of this slab waveguide configuration. The final expression should have the form

$$\frac{2\kappa\gamma}{\kappa^2 - \gamma^2} = \tan(\kappa\rho) \quad \text{with} \quad \gamma = \gamma_1 = \gamma_3. \quad (2.9)$$

Solution:

We start by equating equations (2.7), (2.8) and using $C\gamma_3 = B\kappa$

$$\begin{aligned} B \sin(\kappa\rho) + C \cos(\kappa\rho) &= \frac{C\kappa}{\gamma_1} \sin(\kappa\rho) - \frac{B\kappa}{\gamma_1} \cos(\kappa\rho) \\ \Rightarrow B \sin(\kappa\rho) + \frac{\kappa}{\gamma_3} B \cos(\kappa\rho) &= \frac{B\kappa^2}{\gamma_1\gamma_3} \sin(\kappa\rho) - \frac{B\kappa}{\gamma_1} \cos(\kappa\rho) \\ \Rightarrow \left(1 - \frac{\kappa^2}{\gamma_1\gamma_3}\right) \sin(\kappa\rho) &= -\kappa \left(\frac{1}{\gamma_1} + \frac{1}{\gamma_3}\right) \cos(\kappa\rho) \\ \Rightarrow \frac{\gamma_1\gamma_3 - \kappa^2}{\gamma_1\gamma_3} \sin(\kappa\rho) &= -\kappa \left(\frac{\gamma_1 + \gamma_3}{\gamma_1\gamma_3}\right) \cos(\kappa\rho) \\ \Rightarrow \tan(\kappa\rho) &= \kappa \frac{\gamma_1 + \gamma_3}{\kappa^2 - \gamma_1\gamma_3} = \frac{2\kappa\gamma}{\kappa^2 - \gamma^2}. \end{aligned} \quad (2.10)$$

2.4 Effective indices

Plot the right- and left-handed side of the dispersion equation as a function of n_{eff} for $\rho = 5 \mu\text{m}$, $\lambda_0 = 1 \mu\text{m}$, $n_{\text{co}} = 1.5$, $n_{\text{cl}} = 1.45$ within the range $n_{\text{cl}} < n_{\text{eff}} < n_{\text{co}}$. Remember that $n_{\text{eff}} = \frac{\beta}{k_0}$. Find or read off the effective indices of the fundamental mode and the two next higher-order modes.

We can modify the relations (2.4) as a function of the effective index

$$\kappa^2 = k_0^2(n_{\text{co}}^2 - n_{\text{eff}}^2) \quad \text{and} \quad \gamma^2 = k_0^2(n_{\text{eff}}^2 - n_{\text{cl}}^2). \quad (2.11)$$

Substituting this into (2.10) results in

$$\tan\left(k_0\rho\sqrt{n_{\text{co}}^2 - n_{\text{eff}}^2}\right) = \frac{2\sqrt{(n_{\text{co}}^2 - n_{\text{eff}}^2)(n_{\text{eff}}^2 - n_{\text{cl}}^2)}}{(n_{\text{co}}^2 - n_{\text{eff}}^2) - (n_{\text{eff}}^2 - n_{\text{cl}}^2)} = \frac{2\sqrt{(n_{\text{co}}^2 - n_{\text{eff}}^2)(n_{\text{eff}}^2 - n_{\text{cl}}^2)}}{n_{\text{co}}^2 - 2n_{\text{eff}}^2 + n_{\text{cl}}^2}. \quad (2.12)$$

We can now find the solutions in a graphical way as displayed in figure 5.

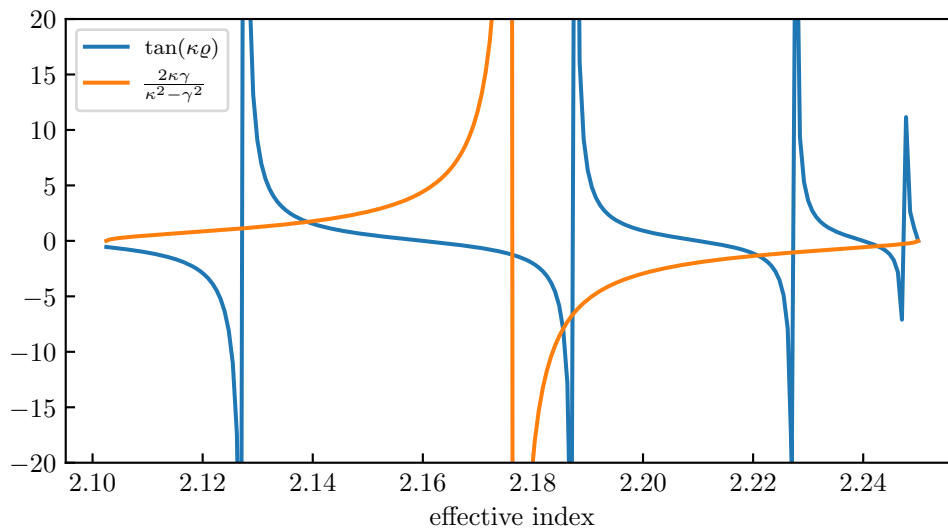


Fig. 5: Plot of the left hand side and right hand side of (2.12). The three solutions we can obtain are $n_1 = 2.139$ (fundamental mode), $n_3 = 2.220$ (first higher mode), $n_4 = 2.242$ (second higher mode).

2.5 Poynting vector

Calculate the transverse Poynting vector distribution of the three modes discussed in the previous task. Use $S_z = \frac{1}{2} \text{Re}(\mathbf{E} \times \mathbf{H}^*)$.

Solution:

We can rewrite the Poynting vector using $|\mathbf{H}| = \frac{n_{\text{eff}}}{c_0\mu_0} |\mathbf{E}|$

$$S_z = \frac{1}{2} \text{Re}(\mathbf{E} \times \mathbf{H}^*) = \frac{n_{\text{eff}}}{c_0\mu_0} |\mathbf{E}|^2 = \frac{\epsilon_0 n_{\text{eff}}}{2} |\mathbf{E}|^2. \quad (2.13)$$

3 Optical fiber

3.1 Transverse EM-components

Show that all transverse EM-components depend on the longitudinal components E_z and H_z . Use Maxwells equations

$$\vec{\nabla} \times \mathbf{H} = -i\omega\epsilon\epsilon_0\mathbf{E} \quad \text{and} \quad \vec{\nabla} \times \mathbf{E} = i\omega\mu_0\mathbf{H} \quad (3.1)$$

in cylindrical coordinates.

Solution:

We start by explicitly writing down the curl operator in cylindrical coordinates

$$\left[\frac{1}{r} \frac{\partial H_z}{\partial \varphi} - \frac{\partial H_\varphi}{\partial z} \right] \hat{\mathbf{e}}_r + \left[\frac{\partial H_r}{\partial z} - \frac{\partial H_z}{\partial r} \right] \hat{\mathbf{e}}_\varphi + \frac{1}{r} \left[\frac{\partial}{\partial r} (r H_\varphi) - \frac{\partial H_r}{\partial \varphi} \right] \hat{\mathbf{e}}_z = -i\omega\epsilon\epsilon_0\mathbf{E} \quad (3.2)$$

$$\left[\frac{1}{r} \frac{\partial E_z}{\partial \varphi} - \frac{\partial E_\varphi}{\partial z} \right] \hat{\mathbf{e}}_r + \left[\frac{\partial E_r}{\partial z} - \frac{\partial E_z}{\partial r} \right] \hat{\mathbf{e}}_\varphi + \frac{1}{r} \left[\frac{\partial}{\partial r} (r E_\varphi) - \frac{\partial E_r}{\partial \varphi} \right] \hat{\mathbf{e}}_z = i\omega\mu_0\mathbf{H}. \quad (3.3)$$

Furthermore we want to assume fields of the form $E(x, y, z) = u(x, y)e^{i\beta z}$ with a phase factor $\beta = n_{\text{eff}}k_0$. From that we can read of the transverse components of electric and magnetic field:

$$E_r = \frac{i}{\omega\epsilon\epsilon_0} \left[\frac{1}{r} \frac{\partial H_z}{\partial \varphi} - i\beta H_\varphi \right] \quad E_\varphi = \frac{i}{\omega\epsilon\epsilon_0} \left[i\beta H_r - \frac{\partial H_z}{\partial r} \right] \quad (3.4)$$

$$H_r = \frac{1}{i\omega\mu_0} \left[\frac{1}{r} \frac{\partial E_z}{\partial \varphi} - i\beta E_\varphi \right] \quad H_\varphi = \frac{1}{i\omega\mu_0} \left[i\beta E_r - \frac{\partial E_z}{\partial r} \right]. \quad (3.5)$$

For the radial component of the electric field (3.4) we substitute the φ component of the magnetic field (3.5) and find with $k_0 = \omega/c_0$

$$E_r = \frac{i}{\omega\epsilon\epsilon_0} \left[\frac{1}{r} \frac{\partial H_z}{\partial \varphi} - \frac{\beta}{\omega\mu_0} \left[i\beta E_r - \frac{\partial E_z}{\partial r} \right] \right]$$

$$\underbrace{\left(1 - \frac{\beta^2}{\omega^2\epsilon\epsilon_0\mu_0} \right)}_{1 - \frac{n_{\text{eff}}^2}{\epsilon}} E_r = \frac{i}{\omega\epsilon\epsilon_0} \left[\frac{1}{r} \frac{\partial H_z}{\partial \varphi} + \frac{\beta}{\omega\mu_0} \frac{\partial E_z}{\partial r} \right] \quad \text{with} \quad c_0^2 = \frac{1}{\mu_0\epsilon_0}$$

$$E_r = \frac{ic_0}{\omega\epsilon} \frac{1}{1 - \frac{n_{\text{eff}}^2}{\epsilon}} \left[\frac{1}{\epsilon_0 c_0 r} \frac{\partial H_z}{\partial \varphi} + \frac{\beta}{\omega c_0 \mu_0 \epsilon_0} \frac{\partial E_z}{\partial r} \right]$$

$$E_r = \frac{i}{k_0(\epsilon - n_{\text{eff}}^2)} \left[\frac{1}{\epsilon_0 c_0 r} \frac{\partial H_z}{\partial \varphi} + n_{\text{eff}} \frac{\partial E_z}{\partial r} \right]. \quad (3.6)$$

We can also find the φ component of the magnetic field by substituting E_r instead

$$\begin{aligned}
H_\varphi &= \frac{1}{i\omega\mu_0} \left[-\frac{\beta}{\omega\varepsilon\varepsilon_0} \left[\frac{1}{r} \frac{\partial H_z}{\partial \varphi} - i\beta H_\varphi \right] - \frac{\partial E_z}{\partial r} \right] \\
\left(1 - \frac{\beta^2}{\omega^2\mu_0\varepsilon_0\varepsilon}\right) H_\varphi &= \frac{1}{i\omega\mu_0} \left[-\frac{\beta}{\omega\varepsilon\varepsilon_0} \frac{1}{r} \frac{\partial H_z}{\partial \varphi} - \frac{\partial E_z}{\partial r} \right] \\
\left(1 - \frac{n_{\text{eff}}^2}{\varepsilon}\right) H_\varphi &= \frac{ic_0}{\omega\varepsilon} \left[-\frac{\beta}{\omega c_0\mu_0\varepsilon_0} \frac{1}{r} \frac{\partial H_z}{\partial \varphi} - \frac{\varepsilon}{c_0\mu_0} \frac{\partial E_z}{\partial r} \right] \\
H_\varphi &= \frac{-i}{k_0(\varepsilon - n_{\text{eff}}^2)} \left[\frac{n_{\text{eff}}}{r} \frac{\partial H_z}{\partial \varphi} + \varepsilon\varepsilon_0 c_0 \frac{\partial E_z}{\partial r} \right]. \tag{3.7}
\end{aligned}$$

The other two components can be derived analogously and are:

$$\begin{aligned}
E_\varphi &= -K \left(-\frac{n_{\text{eff}}}{r} \frac{\partial E_z}{\partial \varphi} + \frac{1}{\varepsilon_0 c_0} \frac{\partial H_z}{\partial r} \right) \\
H_r &= K \left(n_{\text{eff}} \frac{\partial H_z}{\partial r} - \frac{\varepsilon\varepsilon_0 c_0}{r} \frac{\partial E_z}{\partial \varphi} \right) \quad \text{with} \quad K = \frac{i}{k_0(\varepsilon - n_{\text{eff}}^2)}. \tag{3.8}
\end{aligned}$$

3.2 Application of boundary conditions

Use boundary condition BC3 ($A = A_E$) and BC4 ($A = A_H$) to find expressions for A . Use the relation

$$J'_m(x) = \frac{m}{x} J_m(x) - J_{m+1}(x) \quad \text{and} \quad K'_m(x) = \frac{m}{x} K_m(x) - K_{m+1}(x). \tag{3.9}$$

Solution:

We start by writing down the two boundary conditions

$$\text{BC3: } E_\varphi^{\text{co}} = E_\varphi^{\text{cl}} \quad \text{BC4: } H_\varphi^{\text{co}} = H_\varphi^{\text{cl}} \tag{3.10}$$

Furthermore we want to list again the ansatz functions for the z -component of the fields: Now we take the expressions from Task 1 and insert the ansatz vor the fields E_z and H_z . We

Table 1: Ansatz functions for the longitudinal fields. Note that $B = 1$ since only the ratio between A and B is relevant.

	E_z	H_z
core	$A \frac{J_m(UR)}{J_m(U)} \cos(m\varphi)$	$B \frac{J_m(UR)}{J_m(U)} \sin(m\varphi)$
cladding	$A \frac{K_m(WR)}{K_m(W)} \cos(m\varphi)$	$B \frac{K_m(WR)}{K_m(W)} \sin(m\varphi)$

start with BC3 ($r = \rho, R = 1$)

$$\begin{aligned}
E_\varphi^{\text{co}} &= -K_{\text{co}} \left(-\frac{n_{\text{eff}}}{r} \frac{\partial E_z}{\partial \varphi} + \frac{1}{\varepsilon_0 c_0} \frac{\partial H_z}{\partial r} \right) \\
&= -K_{\text{co}} \left(-\frac{n_{\text{eff}}}{r} \frac{\partial}{\partial \varphi} [A_E \cos(m\varphi)] + \frac{1}{\varepsilon_0 c_0} \frac{\partial}{\partial r} \left[\frac{J_m(U)}{J_m(U)} \sin(m\varphi) \right] \right) \\
&= -K_{\text{co}} \left(\frac{n_{\text{eff}}}{r} m A_E \sin(m\varphi) + \frac{1}{\varepsilon_0 c_0 \rho} \sin(m\varphi) \left[m - \frac{J_{m+1}(U)}{J_m(U)} U \right] \right) \\
E_\varphi^{\text{cl}} &\stackrel{!}{=} -K_{\text{cl}} \left(\frac{n_{\text{eff}}}{r} m A_E \sin(m\varphi) + \frac{1}{\varepsilon_0 c_0 \rho} \sin(m\varphi) \left[m - \frac{K_{m+1}(W)}{K_m(W)} W \right] \right). \tag{3.11}
\end{aligned}$$

We can solve this equation for A_E

$$\begin{aligned}
A_E &= \frac{\frac{\sin(m\varphi)}{\varepsilon_0 c_0 \rho} \left(-\frac{K_{m+1}(W)}{K_m(W)} W + \frac{J_{m+1}(U)}{J_m(U)} U \right)}{\frac{n_{\text{eff}}}{\rho} m \sin(m\varphi) (K_{\text{cl}} - K_{\text{co}})} \\
&= \frac{1}{\varepsilon_0 c_0 n_{\text{eff}} m (K_{\text{cl}} - K_{\text{co}})} \left(K_{\text{cl}} \frac{K_{m+1}(W)}{K_m(W)} W - K_{\text{co}} \frac{J_{m+1}(U)}{J_m(U)} U \right). \tag{3.12}
\end{aligned}$$

We repeat all steps with BC4 ($r = \rho, R = 1$)

$$\begin{aligned}
H_\varphi^{\text{co}} &= K_{\text{co}} \left(\frac{n_{\text{eff}}}{\rho} m \cos(\varphi) + \varepsilon_0 c_0 \varepsilon_{\text{co}} \frac{A_H}{\rho} \cos(m\varphi) \left[m - \frac{J_{m+1}(U)}{J_m(U)} U \right] \right) \\
H_\varphi^{\text{cl}} &\stackrel{!}{=} K_{\text{cl}} \left(\frac{n_{\text{eff}}}{\rho} m \cos(\varphi) + \varepsilon_0 c_0 \varepsilon_{\text{cl}} \frac{A_H}{\rho} \cos(m\varphi) \left[m - \frac{K_{m+1}(W)}{K_m(W)} W \right] \right). \tag{3.13}
\end{aligned}$$

Again, solving for A_H yields

$$A_H = \frac{(K_{\text{cl}} - K_{\text{co}}) n_{\text{eff}} m}{\varepsilon_0 c_0 \left[m(\varepsilon_{\text{co}} - \varepsilon_{\text{cl}}) + K_{\text{cl}} \varepsilon_{\text{cl}} \frac{K_{m+1}(W)}{K_m(W)} W - K_{\text{co}} \varepsilon_{\text{co}} \frac{J_{m+1}(U)}{J_m(U)} U \right]}. \tag{3.14}$$

3.3 Dispersion relation

Determine the dispersion relation of the optical fiber by setting $A_E = A_H$.

Solution:

We first start by rewriting K_{co} and K_{cl} in terms of U and W

$$\begin{aligned}
U^2 &= \rho^2 (k_0^2 \varepsilon_{\text{co}} - \beta^2) \quad \Rightarrow \quad K_{\text{co}} = \frac{k_0 \rho^2 i}{U^2} \\
W^2 &= \rho^2 (k_0^2 \varepsilon_{\text{cl}} - \beta^2) \quad \Rightarrow \quad K_{\text{cl}} = -\frac{k_0 \rho^2 i}{W^2}. \tag{3.15}
\end{aligned}$$

Then we equate (3.12) and (3.14)

$$\begin{aligned}
(K_{\text{cl}} - K_{\text{co}})^2 (n_{\text{eff}} m)^2 &= \left[K_{\text{cl}} \frac{K_{m+1}(W)}{K_m(W)} W - K_{\text{co}} \frac{J_{m+1}(U)}{J_m(U)} U \right] \\
&\quad \left[m(\epsilon_{\text{co}} - \epsilon_{\text{cl}}) + K_{\text{cl}} \epsilon_{\text{cl}} \frac{K_{m+1}(W)}{K_m(W)} W - K_{\text{co}} \epsilon_{\text{co}} \frac{J_{m+1}(U)}{J_m(U)} U \right] \\
\left(\frac{1}{U^2} + \frac{1}{W^2} \right)^2 (n_{\text{eff}} m)^2 &= \left[-\frac{K_{m+1}(W)}{W K_m(W)} - \frac{J_{m+1}(U)}{U J_m(U)} \right] \\
&\quad \left[m(\epsilon_{\text{co}} - \epsilon_{\text{cl}}) - \epsilon_{\text{cl}} \frac{K_{m+1}(W)}{W K_m(W)} - \epsilon_{\text{co}} \frac{J_{m+1}(U)}{U J_m(U)} \right] \\
\left(\frac{V}{UW} \right)^4 \left(\frac{n_{\text{eff}} m}{n_{\text{co}}} \right)^2 &= \left[\frac{K_{m+1}(W)}{W K_m(W)} + \frac{J_{m+1}(U)}{U J_m(U)} \right] \\
&\quad \left[m(\epsilon_{\text{cl}} - \epsilon_{\text{co}}) - \left(\frac{n_{\text{cl}}}{n_{\text{co}}} \right)^2 \frac{K_{m+1}(W)}{W K_m(W)} + \frac{J_{m+1}(U)}{U J_m(U)} \right]. \tag{3.16}
\end{aligned}$$

4 Weakly guiding fibers

4.1 Cut-off condition

Show that in weakly guidance approximation, the cut-off condition for the first higher-order mode is given by $0 = J_0(V)$.

Solution:

We can use the dispersion equation of weakly guided fiber modes

$$\frac{UJ_{l-1}(U)}{J_l(U)} = -\frac{WK_{l-1}(W)}{K_l(W)}, \quad (4.1)$$

where we consider the first order solution ($l = 1$). At the cut-off the modes get completely localized. This happens when $W^2 \propto \beta^2 - k_0^2 n_{cl}^2 = 0$ and thus $U = V$. Then we find

$$\frac{UJ_0(U)}{J_1(U)} = 0 \Rightarrow J_0(V) = 0 \quad \text{for } V \neq 0. \quad (4.2)$$

4.2 Cut-off numbers

Show that the cut-off numbers are given by $X_{lm} = (l + 2m)\frac{\pi}{2}$, using the approximation

$$J_l(X) = \sqrt{\frac{2}{\pi X}} \cos\left(X - \left(l + \frac{1}{2}\right)\frac{\pi}{2}\right), \quad (4.3)$$

which holds for large values of X (multi-mode fiber).

Solution:

From the first task the cut-off condition is given by $J_l(X) = 0$. Thus we set (4.3) to zero and find

$$\begin{aligned} 0 &= \cos\left(X - \left(l + \frac{1}{2}\right)\frac{\pi}{2}\right) \\ \Rightarrow m\pi + \frac{\pi}{2} &= X - \left(l + \frac{1}{2}\right)\frac{\pi}{2} \\ \Rightarrow X &= \frac{\pi}{2}\left(2m + l + \frac{3}{2}\right). \end{aligned} \quad (4.4)$$

For large values of X the term $3/2$ can be neglected compared to the other terms. This leads to

$$X = \frac{\pi}{2}(2m + l). \quad (4.5)$$

4.3 Effective index

Show that the propagation constant is analytic, using the definition of U and the assumption that $U = X_{lm}$ (vertical lines in dispersion function diagram).

Plot n_{eff} first as a function of m for $l = 0$ ($1 \leq m \leq 5$) and second as function of l for $m = 1$ ($0 \leq l \leq 4$) using $n_1 = 1.5$, $\rho = 50 \mu\text{m}$, $\lambda = 1 \mu\text{m}$. What can you say about the phase velocity?

Solution:

We use the definition of U and try to solve for β

$$\begin{aligned} \frac{\pi}{2}(2m+l) &= \rho \sqrt{k_0^2 n_{\text{co}}^2 - \beta^2} \\ \beta^2 &= k_0^2 n_{\text{co}}^2 - \frac{\pi^2}{4\rho^2} (2m+l)^2. \end{aligned} \quad (4.6)$$

Now using $\beta = n_{\text{eff}} k_0$ we can conclude

$$n_{\text{eff}} = \sqrt{n_{\text{co}}^2 - \left(\frac{\pi}{2\rho k_0}\right)^2 (2m+l)^2}. \quad (4.7)$$

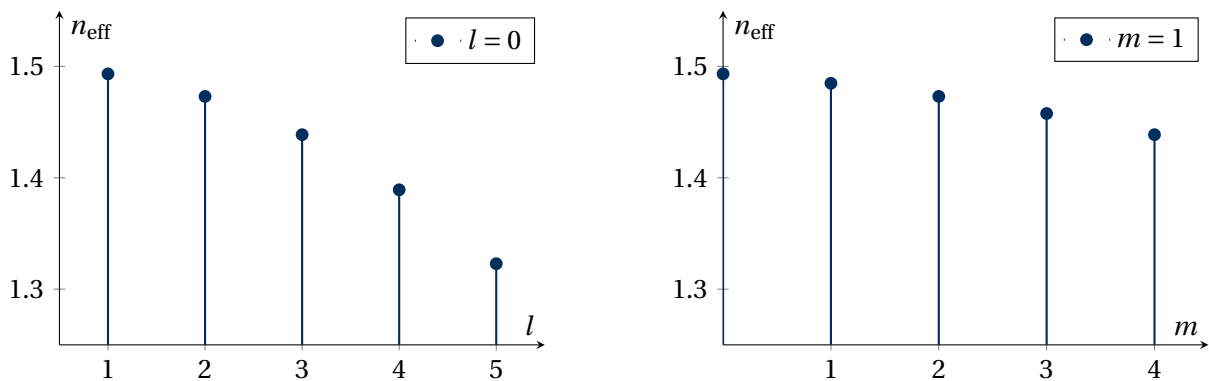


Fig. 6: Effective index of the weakly guided fiber for constant $l = 0$ (left) as a function of m and for constant $m = 1$ as a function of l .

By looking at figure 6 we conclude that the effective index decreases for higher order modes. Since the phase velocity $v_p = c/n_{\text{eff}}$ is inversely proportional to the effective index, it will increase for higher modes.

4.4 Group velocity

Derive an analytic expression for the group velocity, assuming that n_1 is wavelength independent.

Solution:

The group velocity is given as $v_g = d\omega/d\beta$. We start with (4.6) and take the total derivative

$$\begin{aligned}\beta^2 &= \frac{n_{co}^2}{c^2} \omega^2 - \frac{\pi^2}{4\rho^2} (2m+l)^2 \\ 2\beta d\beta &= \frac{n_{co}^2}{c^2} 2\omega d\omega \\ \Rightarrow v_g = \frac{d\omega}{d\beta} &= \frac{c}{n_{co}^2} \frac{\beta}{k_0} = \frac{c}{n_{co}^2} \sqrt{n_{co}^2 - \left(\frac{\pi}{2\rho k_0}\right)^2 (2m+l)^2}.\end{aligned}\quad (4.8)$$

Since the group velocity is proportional to the effective index, it will decrease for higher order modes.

5 Pulse propagation

5.1 Pulse envelope without dispersion

Derive the pulse envelope for the case of vanishing group velocity dispersion (GVD) in the situation of a Gaussian pulse at input given by

$$F(t') = e^{-\left(\frac{t'}{\tau_p}\right)^2} e^{-i\omega_0 t'}. \quad (5.1)$$

Solution:

We start with the Fourier analysis as done in the lecture

$$F(z, t) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} \tilde{F}(z, \omega) e^{-i\omega t} d\omega, \quad (5.2)$$

where $\tilde{F}(z, \omega)$ is the Fourier component of $F(z, t)$ at the frequency ω . In the frequency domain we know the spatial evolution of $\tilde{F}(z, \omega)$ namely

$$\tilde{F}(z, \omega) = \tilde{F}(0, \omega) e^{i\beta(\omega)z} \quad \text{with} \quad \tilde{F}(0, \omega) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} F(0, t) e^{i\omega t} dt. \quad (5.3)$$

So then by substituting (5.3) into (5.2) we find

$$F(z, t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} \tilde{F}(0, \omega) e^{i(\beta(\omega)z - i\omega t)} d\omega. \quad (5.4)$$

We start the calculations by first computing the Fourier transform of the input pulse using the Gaussian integral given as

$$\int_{-\infty}^{\infty} dx e^{-ax^2 + bx} = \sqrt{\frac{\pi}{a}} e^{\frac{b^2}{4a}}. \quad (5.5)$$

Then we find by using $\beta(\omega) = \beta_0 + \beta'(\omega - \omega_0)$

$$\begin{aligned} \tilde{F}(0, \omega) &= \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} e^{-\left(\frac{t}{\tau_p}\right)^2} e^{i(\omega - \omega_0)t} dt = \tau_p \sqrt{\pi} e^{-\frac{\tau_p^2}{4}(\omega - \omega_0)^2}, \\ \Rightarrow F(z, t) &= \frac{\tau_p \sqrt{\pi}}{2\pi} \int_{-\infty}^{\infty} d\omega e^{-\frac{\tau_p^2}{4}(\omega - \omega_0)^2} e^{i[(\beta_0 + \beta'(\omega - \omega_0))z - \omega t]}, \end{aligned} \quad (5.6)$$

Now we perform a variable substitution $\bar{\omega} = \omega - \omega_0$ and find

$$F(z, t) = \frac{\tau_p \sqrt{\pi}}{2\pi} e^{\beta_0 z - i\omega_0 t} \int_{-\infty}^{\infty} d\bar{\omega} e^{-\frac{\tau_p^2}{4}\bar{\omega}^2} e^{i[\beta'z - t]\bar{\omega}} \quad (5.7)$$

$$= \exp\left(-\frac{(\beta'z - t)^2}{\tau_p^2}\right) e^{\beta_0 z - i\omega_0 t}. \quad (5.8)$$

5.2 Pulse envelope with dispersion

Derive the same envelope but now assume GVD $\neq 0$.

Solution:

Now with group delay dispersion $\beta_2 \neq 0$ we write $\beta(\omega) = \beta_0 + \beta'(\omega - \omega_0) + \frac{1}{2}\beta''(\omega - \omega_0)^2$ and equation (5.7) modifies to

$$F(z, t) = \frac{\tau_p \sqrt{\pi}}{2\pi} e^{i(\beta_0 z - \omega_0 t)} \int_{-\infty}^{\infty} d\bar{\omega} e^{-\frac{\tau_p^2}{4}\bar{\omega}^2} e^{i[\frac{1}{2}\beta'' z \bar{\omega}^2 + (\beta' z - t)\bar{\omega}]}, \quad (5.9)$$

This is formally solved by setting $a = \frac{\tau_p^2}{4} - \frac{1}{2}\beta'' z$ and $b = i(\beta' z - t)$ in equation (5.5)

$$F(z, t) = \frac{\tau_p}{2} \frac{1}{\sqrt{\frac{\tau_p^2}{4} - \frac{1}{2}\beta'' z}} \exp\left(-\frac{(\beta' z - t)^2}{\tau_p^2 + 2i\beta'' z}\right) e^{i(\beta_0 z - \omega_0 t)} \quad (5.10)$$

5.3 Pulse width

Derive the position dependent pulse width and show that by using a pulse width level of $B = e^{-1/4}$, the following equation results:

$$\tau(z) = \tau_p \sqrt{1 + \left(\frac{2z\beta_2}{\tau_p^2}\right)^2}. \quad (5.11)$$

Solution:

In order to find the pulse width we need to split the exponential in equation (5.10) into amplitude and phase

$$F(z, t) = \underbrace{\frac{1}{\sqrt{1 - i\frac{2\beta_2 z}{\tau_p^2}}}}_{\text{amplitude change}} \underbrace{\exp\left(-\frac{(t - z\beta_1)^2 \tau_p^2}{4z^2 \beta_2^2 + \tau_p^4}\right)}_{\text{width change}} \underbrace{\exp\left(i\frac{2z\beta_2(t - z\beta_1)}{4z^2 \beta_2^2 + \tau_p^4}\right)}_{\text{local phase influence}} \underbrace{e^{i(\beta_0 z - \omega_0 t)}}_{\text{carrier phase}}. \quad (5.12)$$

We only need to consider the change of width described by the real part of the exponential term. For a pulse width level $B = e^{-1/4}$ we demand

$$\frac{\tau_p^2}{4z^2 \beta_2^2 + \tau_p^4} \stackrel{!}{=} \frac{1}{\tau(z)^2}. \quad (5.13)$$

Now we simply solve for $\tau(z)$

$$\tau(z) = \sqrt{\frac{4z^2 \beta_2^2 + \tau_p^4}{\tau_p^2}} = \tau_p \sqrt{1 + \left(\frac{2z\beta_2}{\tau_p^2}\right)^2}. \quad (5.14)$$

5.4 Cross over position for different initial pulse lengths

Determine the cross-over position at which a pulse of initial width τ_p^a has a larger temporal pulse width than a pulse with $(\tau_p^b < \tau_p^a)$. Assume the same GVD.

Solution:

Using (5.14) we can equate the two equations for different initial pulse lengths and solve for z

$$\begin{aligned}
 \tau_p^a \sqrt{1 + \left(\frac{2z\beta_2}{\tau_p^a}\right)^2} &= \tau_p^b \sqrt{1 + \left(\frac{2z\beta_2}{\tau_p^b}\right)^2} \\
 \Rightarrow (\tau_p^a)^2 - (\tau_p^b)^2 &= (2z\beta_2)^2 \left(\frac{1}{(\tau_p^b)^2} - \frac{1}{(\tau_p^a)^2} \right) \\
 \Rightarrow z^2 &= \frac{1}{4\beta_2^2} \frac{(\tau_p^a)^2 - (\tau_p^b)^2}{\frac{1}{(\tau_p^b)^2} - \frac{1}{(\tau_p^a)^2}} \\
 \Rightarrow z &= \frac{\tau_p^a \tau_p^b}{2\beta_2}. \tag{5.15}
 \end{aligned}$$